

How Softness Contributes to Human Dexterity



Shinichi Hirai
Dept. Robotics, Ritsumeikan Univ.
<http://www.ritsumeai.ac.jp/se/~hirai/>

Why human dexterity



Humans exhibit outstanding dexterity

Science source of dexterity

Engineering dexterous hands

Background (1/3)

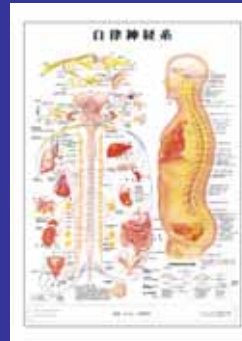


Humans exhibit outstanding dexterity

What's the sources of dexterity

brain-nerve system
binocular eyes
tactile receptors
else?

Background (2/3)



Brain-nerve system

delay in signal transmission
(30 – 50 ms)

Why humans can manipulate objects despite of delay?

Background (3/3)



Human finger
soft fingertip
hard fingernail on the reverse side

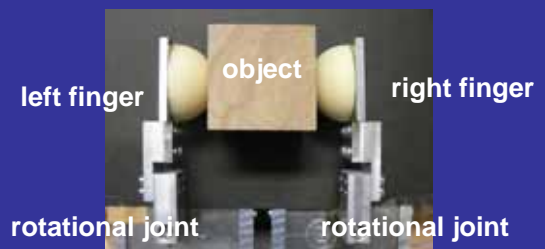
Differs from animals

Does this structure contribute to dexterity?



Observations (1/4)

Ability of a pair of 1-DOF fingers with hemispherical soft tips and hard back plates



Observations (2/4)

move two fingertips inward



small deformation (grasping force)



large deformation (grasping force)

Can control grasping force

Observations (3/4)

rotate two fingertips in the same direction



Can control object posture

Observations (4/4)

Fix two fingers and apply external force to pinched object



Object rotates without slip

Findings from observations

A pair of 1-DOF fingers with soft tips

can control grasping force and object posture independently against Arimoto et al.'s claim

grasped object can rotate even if the two fingers are fixed

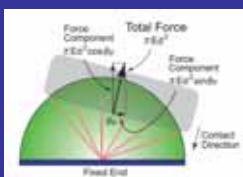
Model compatible with the observations

Modeling (1/7)



Arimoto et al.

A pair of 1 DOF fingers cannot control object posture

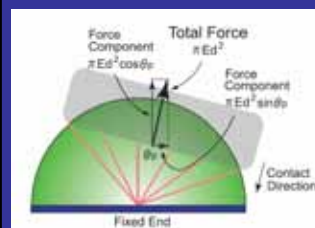


Discrepancy between the observation and the claim

Based on **radially distributed model**

Modeling (2/7)

Radially distributed model



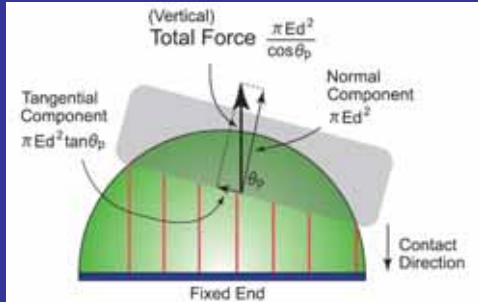
Contact force passes the center of hemisphere

Two fingertips cause non-zero moment around the object

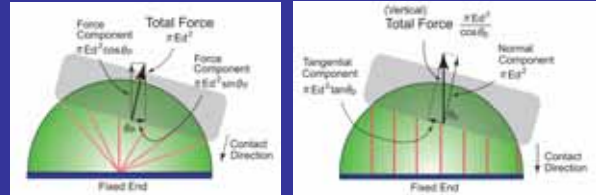
The **3rd DOF** to cancel out the moment

Modeling (3/7)

Parallel distributed model



Modeling (4/7)



radial

parallel

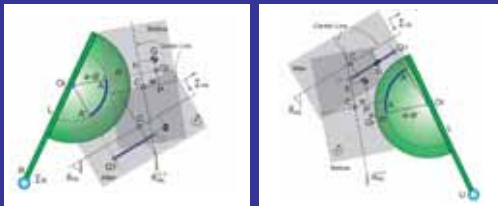
$$F_{\text{radial}} = \pi E d^2$$

$$F_{\text{perp}} = \frac{\pi E d^2}{\cos \theta_p}$$

Force depends on object posture

Modeling (5/7)

Rolling constraints



left fingertip

right fingertip

Object posture is unique (the object cannot rotate) when two fingers are fixed

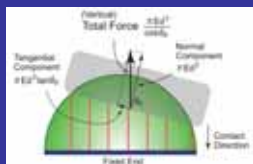
Modeling (6/7)

Parallel distributed model with tangential deformation



$$F_{\text{tangent}} = 2\pi E d d_t$$

Modeling (7/7)



$$U_{\text{parallel}}(d, d_t, \theta_p) = U_{\text{perp}}(d, \theta_p) + U_{\text{tangent}}(d, d_t, \theta_p)$$

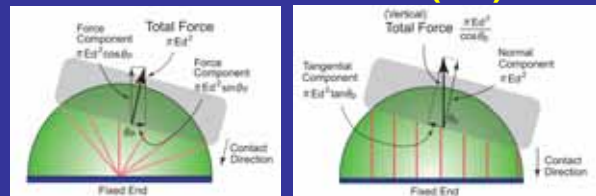
$$U_{\text{perp}}(d, \theta_p) = \frac{\pi E d^3}{3 \cos^2 \theta_p}$$

normal

$$U_{\text{tangent}}(d, d_t, \theta_p) = \pi E \{ d^2 d_t \tan \theta_p + d d_t^2 \}$$

tangential

Model verification (1/2)



radial

parallel

$$F_{\text{radial}} = \pi E d^2$$

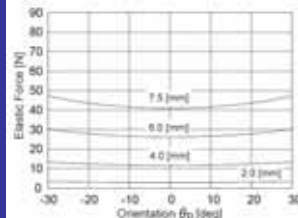
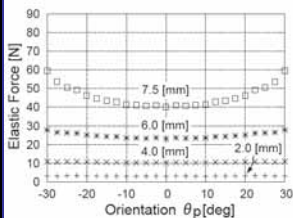
$$F_{\text{perp}} = \frac{\pi E d^2}{\cos \theta_p}$$

Examine if force depends on object posture

Model verification (2/2)



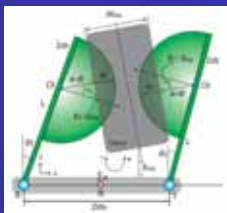
parallel model



Experiment



Simulation (1/3)



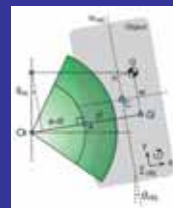
dynamic simulation based on Lagrange formulation kinetic and potential energies

object
left fingertip right fingertip

$$T = \frac{1}{2} m_{obj} (\dot{x}_{obj}^2 + \dot{y}_{obj}^2) + \frac{1}{2} I_{obj} \dot{\theta}_{obj}^2 + \frac{1}{2} I_{finger} \dot{\theta}_1^2 + \frac{1}{2} I_{finger} \dot{\theta}_2^2$$

$$U = U_{parallel}(d_{n1}, d_{t1}, \theta_1 - \theta_{obj}) + U_{parallel}(d_{n2}, d_{t2}, \theta_2 + \theta_{obj}) + m_{obj} g y_{obj}$$

Simulation (2/3)



normal constraints (holonomic)

$$C_1^H \triangleq -(x_{obj} - O_{1x})C_{obj} - (y_{obj} - O_{1y})S_{obj} - (a - d_{n1}) + \frac{W_{obj}}{2} = 0$$



rolling constraints (non-holonomic)

$$C_1^N \triangleq \dot{G}Q_1 + a(\dot{\theta}_1 - \dot{\theta}_{obj}) + \dot{d}_{t1} = 0$$

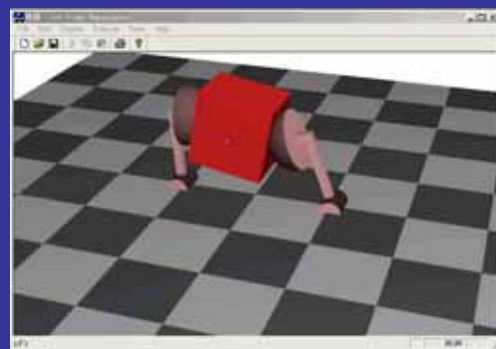
Simulation (3/3)

Lagrangian

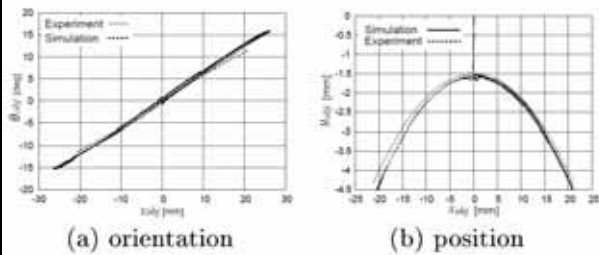
$$\mathcal{L} = T - U + \lambda_1^H C_1^H + \lambda_2^H C_2^H$$

object	}	$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{x}_{obj}} - \frac{\partial \mathcal{L}}{\partial x_{obj}} = \frac{\partial}{\partial x_{obj}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{y}_{obj}} - \frac{\partial \mathcal{L}}{\partial y_{obj}} = \frac{\partial}{\partial y_{obj}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}_{obj}} - \frac{\partial \mathcal{L}}{\partial \theta_{obj}} = \frac{\partial}{\partial \theta_{obj}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$	holonomic non-holonomic
fingertips	}	$\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{d}_{n1}} - \frac{\partial \mathcal{L}}{\partial d_{n1}} = \frac{\partial}{\partial d_{n1}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{d}_{t1}} - \frac{\partial \mathcal{L}}{\partial d_{t1}} = \frac{\partial}{\partial d_{t1}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{d}_{n2}} - \frac{\partial \mathcal{L}}{\partial d_{n2}} = \frac{\partial}{\partial d_{n2}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$ $\frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{d}_{t2}} - \frac{\partial \mathcal{L}}{\partial d_{t2}} = \frac{\partial}{\partial d_{t2}} (\lambda_1^H C_1^H + \lambda_2^H C_2^H)$	normal tangential

Simulation (3/3)

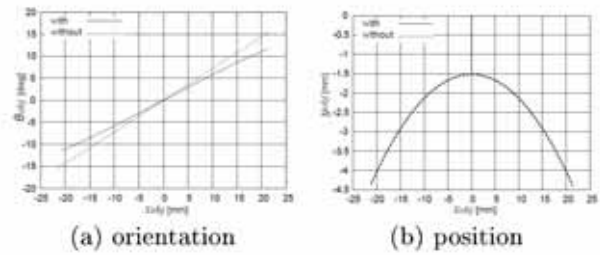


Comparison (1/2)



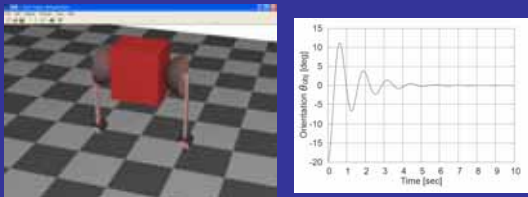
simulation vs experiment

Comparison (2/2)



with / without tangential deformation

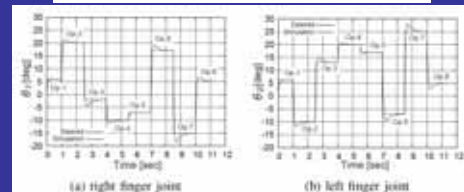
Response to external force



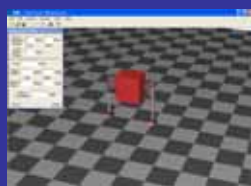
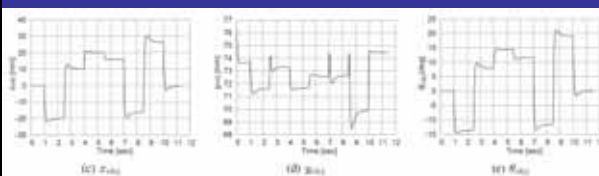
Object rotates without slip as observation
Robust against external force

Finger joint angle control (1/2)

initial state	both fingers grasp an object in parallel
motion 1	$(\theta_1^1, \theta_2^1) = (6 \text{ deg}, 6 \text{ deg})$
motion 2	$(\theta_1^2, \theta_2^2) = (20 \text{ deg}, -10 \text{ deg})$
motion 3	$(\theta_1^3, \theta_2^3) = (-2 \text{ deg}, 13 \text{ deg})$
motion 4	$(\theta_1^4, \theta_2^4) = (-10 \text{ deg}, 20 \text{ deg})$
motion 5	$(\theta_1^5, \theta_2^5) = (-7 \text{ deg}, 17 \text{ deg})$
motion 6	$(\theta_1^6, \theta_2^6) = (17 \text{ deg}, -7 \text{ deg})$
motion 7	$(\theta_1^7, \theta_2^7) = (-15 \text{ deg}, 25 \text{ deg})$
motion 8	$(\theta_1^8, \theta_2^8) = (5 \text{ deg}, 5 \text{ deg})$

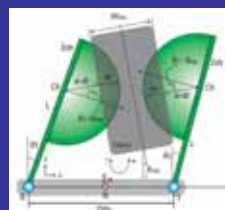


Finger joint angle control (2/2)



Object motion is stabilized without any feedback of object information

Radial vs parallel models



Sum of two fingertip potential energies around equilibrium point with two joints fixed

Radial model --- saddle point

Parallel model --- local minimum

no continuous feedback needed

Rigid vs. soft fingertips



rigid fingertips



soft fingertips

stable grasping	A pair of 1-DOF fingers (2DOF)	A single 1-DOF finger (1DOF)
stable grasping & posture control	1 DOF and 2-DOF fingers (3DOF)	A pair of 1-DOF fingers (2DOF)

Discussion (1/2)

- Parallel distributed model with tangential deformation meets observations
- Experimental model verification force magnitude depends on object posture
- Dynamics of manipulation process simulation and experiment validate parallel model

Discussion (2/2)

- Finger joint angle control object motion is stabilized without object information
- Response to external force meets observations robust against external force

Fingertip model



Is our theory applicable to human manipulation?

Need to measure **inner deformation** of fingertips

Inner deformation

Compute deformation field from MR images before and after deformation

Estimate non-uniform physical parameters from deformation field



MR images

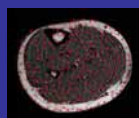
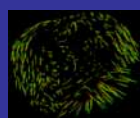


Image processing

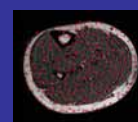


Deformation field

Deformation field computation



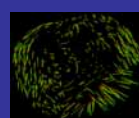
MR images (init. & deformed)



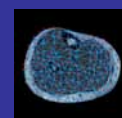
Feature point extraction



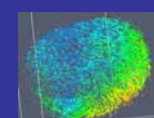
Robust matching



Sparse deformation field



Delaunay triangles/tetrahedra

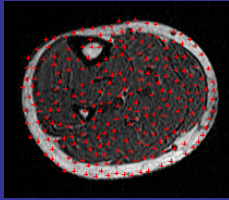


Dense deformation field

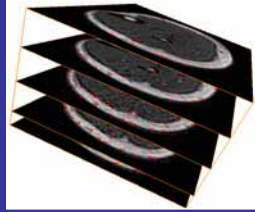
Extracting feature points

3D Harris operator

$$M = \begin{pmatrix} I_x^2 & I_x I_y & I_x I_z \\ I_x I_y & I_y^2 & I_y I_z \\ I_x I_z & I_y I_z & I_z^2 \end{pmatrix}$$



Feature points in one slice



Feature points distributed in layered slices

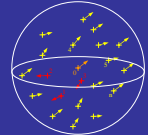
Robust matching

Candidate generation

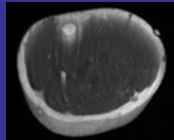
Obtain a set of many-to-many candidate matches using correlation score

Consistency check

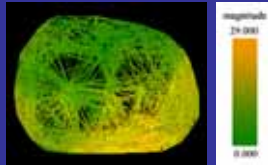
Eliminate false matches so that candidate matches be globally consistent based on energy function



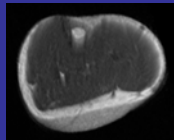
Result



Initial volume (human calf)



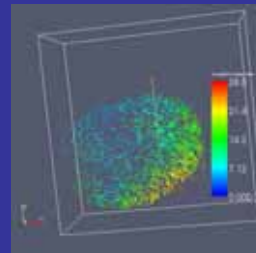
Deformation magnitude at the node of FE model



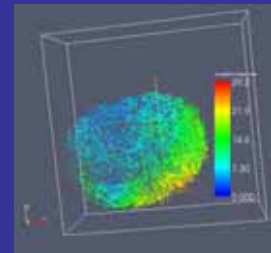
deformed volume

Points in initial volume	1000
Points in deformed volume	5000
Node numbers	771
Tetrahedrons	4344

Result



Deformation Field (10,000 points)

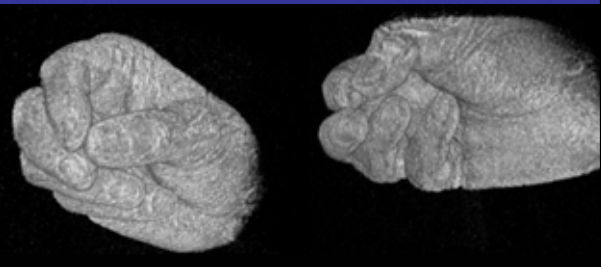


Deformation Field (30,000 points)

Ongoing Issues

- Measuring fingertip deformation during human manipulation
- Simulation of skin deformation
- Identification of physical parameters

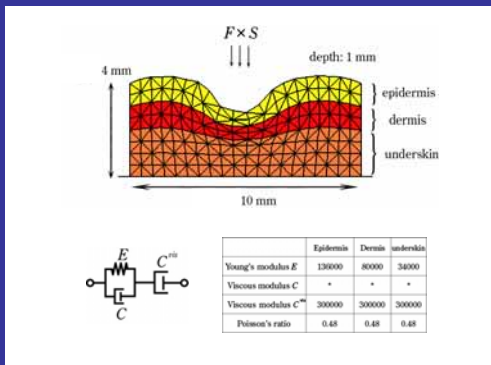
Measuring human fingertips



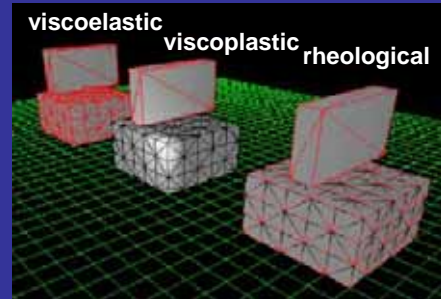
pinch motion

pen grasp

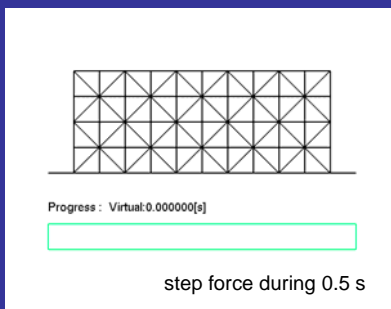
Simulating skin deformation



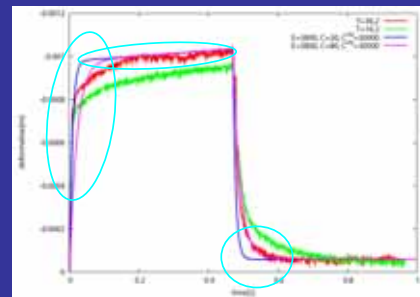
Elastic-plastic deformation



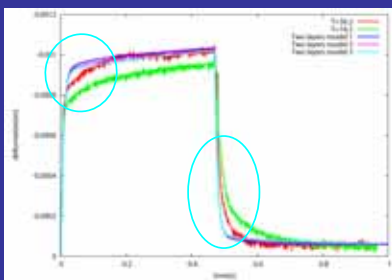
Simulating skin deformation



1-layered model



multi-layered model



20min from Kyoto
70min from Kobe
by local train

Kusatsu
aside of Lake Biwa



Kansai area



Kobe
ICRA2009

Kyoto

Thank you for your attention

